Table 2 Pressure effect on azeotropes in terpolymerization systems

System	P (bar)	f _i	f ₂	f ₃
A	1	0.36(0.40)	0.14(0.06)	0.52(0.54)
	3000	0.38	0.13	0.49
В	1	0.39(0.36)	0.17(0.18)	0.44(0.46)
	3000	0.40	0.17	0.43

The values in brackets refer to the *calculated* values of Wittmer *et al.*¹⁰. There is satisfactory agreement between these values and our experimental data. A, acrylonitrile (1)-diethyl fumarate (2)-styrene (3). B, acrylonitrile (1)-methyl methacrylate (2)- α -methylstyrene (3)



Figure 2 Effect of pressure on the partial azeotropic lines for system C. ____, 1 bar; ____, 3000 bar

carefully examined with other systems. *Partial azeotropy*. The definition of partial azeotropy is given by Ham⁹ as:

$$f_1/f_2 = F_1/F_2; f_2/f_3 = F_2/F_3;$$

$$f_3/f_1 = F_3/F_1$$

where f_1 and F_1 are the molar fractions of monomer 1 in the feed and terpolymer, respectively.

By means of a computer program generating the points defining the azeotropic line for a given monomer, we have calculated the lines of partial azeotropy. The calculation is compared with O'Driscoll's graphic method⁵ using the contour maps. Figure 2 shows partial azeotropic lines for the system, vinyl acetate (M_1) -acrylonitrile (M_2) methyl methacrylate (M_3) . We can see that partial azeotropy is greatly affected by pressure. This is also the case for the first system (not shown here) given in *Table 1* for which, as indicated in Table 2, the coordinates of the ternary azeotrope are not changed by pressure, but partial azeotropic lines are modified by pressure.

In conclusion, the pressure effect in terpolymerization systems can be important with regard to composition and partial azeotropy. However, in the investigated azeotropic systems, the coordinates of the ternary azeotrope are insensitive to pressure. The latter point should be checked for other ternary systems.

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S. Aieche and G. Jenner

Laboratoire de Chimie Organique Appliquée, Institut de Chimie, B.P. 296/R8, 67008 Strasbourg, France (Baseived 20 April 1978; sovied 26 May

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'Moderated copolymerization: 3. Concentration changes in copolymerization with chain transfer: general equations, with special reference to moderated copolymerization' by C. H. Bamford and S. N. Basahel, *Polymer* 1978, **19**, 943–947. Page 946, equation (27) should read:

$$C_{\rm B} = \frac{1}{r_{\rm B}[{\rm B}]_0} \left[\frac{(r_{\rm A}[{\rm A}]_0^2 + 2[{\rm A}]_0[{\rm B}]_0 + r_{\rm B}[{\rm B}]_0^2) \ln\left\{1 - \frac{\Delta({\rm A} + {\rm B})}{[{\rm S}]_0} \left(\frac{1}{\bar{P}_n} - \frac{1}{\bar{P}_n^0}\right)\right\}}{([{\rm A}]_0 + [{\rm B}]_0) \ln\left\{1 - \frac{\Delta({\rm A} + {\rm B})}{[{\rm A}]_0 + [{\rm B}]_0}\right\}} - r_{\rm A} C_{\rm A}[{\rm A}]_0\right]$$

We apologize for this error.